

Article

Metasurface Generation of Paired Accelerating and Rotating Optical Beams for Passive Ranging and Scene Reconstruction

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ABSTRACT: Depth measurements are vital for many emerging technologies with applications in augmented reality, robotics, gesture detection, and facial recognition. These applications, however, demand compact and low-power systems beyond the capabilities of many state-of-the-art depth cameras. While active illumination techniques can enable precise scene reconstruction, they increase power consumption, and systems that employ stereo require extended form factors to separate viewpoints. Here, we exploit a single, spatially multiplexed aperture of nanoscatterers to demonstrate a solution that replicates the functionality of a high-performance depth camera typically comprising a spatial light modulator, polarizer, and multiple lenses. Using cylindrical nanoscatterers that can arbitrarily modify the phase of an incident wavefront, we passively encode two complementary optical responses to depth information in a scene. The designed optical metasurfaces simultaneously generate a focused accelerating beam and a focused rotating beam



that exploit wavefront propagation-invariance to produce paired, adjacent images with a single camera snapshot. Compared to conventional depth from defocus methods, this technique enhances both the depth precision and depth of field at the same time. By decoding the captured data in software, our system produces a fully reconstructed image and transverse depth map, providing an optically passive ranging solution. In our reconstruction algorithm, we account for the field curvature of our metasurface by calculating the change in Gouy phase over the field of view, enabling a fractional ranging error of 1.7%. We demonstrate a precise, visible wavelength, and polarization-insensitive metasurface depth camera with a compact 2 mm² aperture.

KEYWORDS: computational imaging, depth sensors, metasurfaces, extended depth of focus, ranging, wavefront coding

onventional cameras capture two-dimensional projections of intensity information from three-dimensional scenes without any knowledge of depth. While this is often sufficient, depth information is crucial to the operation of numerous nextgeneration technologies, such as autonomous transportation and gesture recognition in augmented reality. A variety of approaches for collecting depth information from a scene exist,^{1,2} but these often require active illumination or multiple viewpoints that prohibitively increase system size. Alternatively, there are depth from defocus methods $^{3-6}$ that obtain depth information from a sequence of images under different defocus settings; however, this typically requires a dynamic setup where the optics are physically adjusted between each capture. Moreover, information theoretic calculations show that the precision from such depth from defocus methods is fundamentally limited for a standard lens,^{7,8} as the point spread function (PSF) varies slowly with changes in depth and it is often ambiguous whether an object is defocused away from or toward the lens.

There are, however, optical elements with more exotic PSFs compared to that of a standard lens, enabling significantly more precise depth discrimination. A prominent example of this is the double-helix PSF (DH-PSF), which distinguishes depths as it produces a beam with two foci that rotate continuously in plane

in response to shifting the distance of a point source.^{8–13} While single-shot depth imaging with a DH-PSF was demonstrated by analyzing an image's power cepstrum,¹⁴ the presence of sidelobes in the PSF limited the reconstructed image quality. The image quality can be improved by capturing an additional reference image, albeit at the cost of not being a single-shot capture.⁸ For real-time depth imaging, this entails physically adjusting the optics and repetitively capturing images. In one implementation of a double-helix-based depth camera,¹³ this functionality was achieved via a spatial light modulator (SLM) whose phase was switched between that of a DH-PSF and a cubic phase mask. This required an extensive setup comprising an imaging lens paired with a polarizer and the SLM, as well as a 4f correlator with two Fourier transform lenses.¹³

Metasurfaces present a compelling route for miniaturizing such systems. These elements consist of quasiperiodic arrays of

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Figure 1. System design. (A) Light from a scene incident on the dual-aperture metasurface will be captured on a sensor as two side-by-side subimages: one of them depth-variant and the other one depth-invariant. These subimages will then be computationally processed to output both a reconstructed scene and a transverse depth map. (B) Schematic of the silicon nitride cylindrical nanoposts on a silicon dioxide substrate. The nanoposts have a lattice constant of *p*, diameter *d*, and thickness *t*. (C) Transmission coefficient (phase and amplitude) as a function of duty cycle for the designed nanoposts. The pillars have a thickness *t* = 600 nm and periodicity *p* = 600 nm.

subwavelength scatterers that can alter the phase, amplitude, and polarization of incident light in an ultrathin form factor,^{15–18} enabling a class of flat lenses.^{19–28} While depth imaging was recently reported using a metasurface-based plenoptic camera,²⁹ this required circularly polarized illumination and relied on small-aperture (21.65 μ m) lenses that limit lateral imaging resolution. Three-dimensional imaging was also demonstrated using a 3 mm aperture design with two interleaved off-axis focusing metalenses,³⁰ but this leveraged the conventional lens PSF from depth from defocus methods, which limits the achievable depth precision.^{7,8} Separately, a metasurface-based DH-PSF³¹ was shown and used for depth imaging,³² but this operated in the infrared, utilized a separate refractive imaging lens, and did not reconstruct the scene. Another work leveraged the chromatic focal shift of a metasurface to acquire object distance information,³³ but this could only accommodate a narrow depth range. In this paper, we demonstrate a miniature, visible wavelength depth camera by collapsing the functionality of multiple supplemental lenses into a single polarizationinsensitive, spatially multiplexed surface with an aperture area of 2 mm². We exploit accelerating and rotating beams together to both extend the depth of field and improve precision. Coupled with deconvolution software, our system generates threedimensional images, i.e., both a transverse depth map and a monochromatic focused scene image with a single snapshot under incoherent, visible illumination.

RESULTS

Our system comprises a dual-aperture metasurface element, consisting of two spatially separated yet adjacent metasurfaces fabricated on the same substrate with distinct and complementary PSFs that work in tandem to enable simultaneous scene reconstruction and depth acquisition (see Figure 1A). These metasurfaces form two separate and nonoverlapping subimages on a sensor array with a single snapshot. The detected subimages

are then processed via a deconvolution algorithm to produce both a focused image and a corresponding depth map. The functionality of the SLM, 4f correlator, and imaging lens present in the standard implementation¹³ are combined into a single surface by setting the phase of each metasurface to a sum of a lens term and a wavefront coding term as

$$\Phi = \Phi_{\text{lens}} + \Phi_{\text{WC}} \tag{1}$$

where λ is the optical wavelength, *x* and *y* are the in-plane position coordinates, and *f* is the focal length of the lens. In our design, both metalenses have a 1 mm wide square aperture, focal length *f* = 5 mm, and a design wavelength λ = 532 nm.

For the first of the two adjacent metasurfaces on the substrate, the wavefront coding term creates an accelerating Airy beam,³ which exhibits a PSF that is highly invariant with depth due to its nondiffracting properties near focus. The wavefront coding term for the second, adjacent metasurface instead creates a rotating beam, which generates a double-helix PSF that is highly sensitive to changes in object depth.¹³ Both metasurfaces are made of silicon nitride cylindrical nanoposts.^{26,35–37} Silicon nitride was selected due to its CMOS compatibility and transparency over the visible wavelength range,³⁸ while cylindrical nanoposts provide the benefit of polarization insensitivity.²² The nanoposts in our design have a thickness t = 600 nm and period p = 400 nm. Figure 1B shows their transmission coefficient as a function of diameter calculated by rigorous coupled-wave analysis³⁹ (see Supporting Information and Figure S1 for transmission coefficient data as a function of lattice constant). Using the simulated transmission coefficient's phase as a lookup table, a diameter is assigned to impart the desired phase for each position in eq 1.

The depth-invariant design is achieved via an extended depth of focus (EDOF) metalens³⁵ with the wavefront coding term



Figure 2. Simulated metasurface point spread functions: The normalized intensities of the simulated PSFs are shown for the EDOF (A) and DH-PSF (B) metalenses for three different object distances. Scale bar: $32 \mu m$.



Figure 3. Fabricated metasurface. (A) Optical image of the metasurface on a glass slide for testing. (B) Optical microscope image of the dual-aperture metasurface. Scale bar: 0.125 mm. Scanning electron micrographs at normal (C) and 45° incidence (D), where the scale bars are 5 μ m and 300 nm, respectively.

$$\Phi_{\rm WC} = \frac{\alpha}{L^3} (x^3 + y^3) \tag{3}$$

where *L* is half the aperture width and α is a constant that multiplies the cubic phase modulation term to generate an accelerating Airy beam that produces a misfocus-insensitive PSF.^{13,35,37,40–42} Figure 2A shows simulated PSFs for the EDOF metalens with $\alpha = 20\pi$ as the point source is shifted to different depths along the optical axis, demonstrating the uniformity in the response. While this metalens does not focus to a point and therefore captures blurry images, by calibration with a single PSF measurement and subsequent deconvolution, focused images can be reconstructed with high quality over a wide depth range.³⁵ This design achieves a resolution of 125 cycles/mm with a highly depth-invariant modulation transfer function compared to a design without the wavefront coding term added (see Supporting Information and Figure S6).

Complementing the depth-invariant design, the depth-variant metasurface creating a rotating beam leverages a DH-PSF. The wavefront coding term of a double-helix metalens is determined via a sum of Laguerre–Gaussian modes^{8,43,44} and a block-iterative weighted projections algorithm^{45–47} (see Supporting Information and Figure S2). Figure 2B shows simulated PSFs for

the designed DH metalens, exhibiting distinct intensity patterns for each depth unlike the case of the EDOF metalens. In an imaging system, the DH metalens creates two spatially shifted and rotated copies of objects, where the rotation angle between the two copies is determined by the distance of the object being imaged.

By calculating the Fisher information with depth, we can assess the information carried by each PSF to understand our system's simultaneous improvement of the depth precision and the depth of field. The Fisher information indicates how sensitive a signal is to a parameter,⁴⁰ in our case, how sensitive each PSF is to depth. High Fisher information means an increase in the depth precision, whereas low Fisher information indicates stronger depth-invariance or an extended depth of field. An ideal, extended depth of field system that is misfocus-insensitive would have zero Fisher information.⁴⁰ Compared to a metalens without any wavefront coding term, our double-helix metalens exhibits 4.6 times the Fisher information averaged over the 10 to 35 cm depth range, whereas the cubic metalens exhibits an average 16.1 times less compared to that of the metalens without any wavefront coding (see Supporting Information, Section S10 and Figure S7, for details). These changes in Fisher information



Figure 4. Metasurface characterization. Normalized measured intensity point spread functions for the EDOF (A) and DH-PSF (B) metalenses for three different object distances. Scale bar: 78 μ m. (C) Orientation angle of the double-helix foci as a function of object distance.



Figure 5. Single-object depth imaging. (A) Raw and unpartitioned image with the double-helix metalens subimage on the left and the EDOF metalens subimage on the right. Scale bar: 0.5 mm. (B) Estimated DH-PSF from the image in (A). Predicted distances compared to the true distances are plotted in (C) for the case of imaging a "3" character at five different distances, where the reconstructed images and depth maps are shown in (D) and (E), respectively. The circles and asterisks in (C) correspond respectively to depth estimates without and with corrections accounting for changes in Gouy phase due to field angle. The red line denotes the performance of a perfect depth estimation algorithm. Scale bars are 78 μ m and 0.2 mm in (B) and (D), respectively.

confirm enhancement of both depth sensitivity and depth of field relative to a clear aperture lens used in a depth from defocus application with the same aperture and focal length.

We then fabricated the dual aperture metasurface to validate our design. Figure 3A shows a picture of the sample mounted on a microscope slide. An optical micrograph of the adjacent metasurfaces in Figure 3B shows the asymmetry in their phase profiles, where the different colored zones correspond to regions of different diameters that were selected to achieve 2π phase coverage. In Figure 3C and D, scanning electron micrographs depict zoomed-in views of the nanoposts on a square lattice at normal and 45° incidence, respectively.

We then measured the PSFs of the fabricated metasurfaces. As expected, the PSF of the EDOF metasurface varied minimally



Figure 6. Imaging multiple objects. (A) Raw and unpartitioned image with the double-helix metalens subimage on the left and the EDOF metalens subimage on the right of a scene with "U" and "W" characters located at different distances. Scale bar: 0.51 mm. (B) Reconstructed object scene with a scale bar of 0.2 mm. Estimated DH-PSFs are shown for the "U" (C) and "W" (D) with scale bars of 78 μ m. (E) Calculated transverse depth map for the scene. (F) Predicted distances compared to the true distances are plotted, where the circles and asterisks correspond respectively to depth estimates without and with corrections accounting for changes in Gouy phase due to field angle. The blue and black points correspond to the "U" and "W" characters, respectively. The red line denotes the performance of a perfect depth estimation algorithm.

with depth (Figure 4A), while that of the DH metalens (Figure 4B) strongly depended on the point source distance, demonstrating a large change ($\sim 87^{\circ}$) in orientation angle over the measured depth range (Figure 4C). Furthermore, the orientation angle of the lobes in the measured DH-PSFs as a function of depth agrees very well with the theory^{8,43} (see Supporting Information). The measured diffraction and transmission efficiencies of the full combined metasurface aperture were 75% and 91%, respectively.

Armed with our dual metasurface aperture exhibiting complementary depth responses, we performed a computational imaging experiment on a scene consisting of patterns on standard printer paper located at different depths. Our patterns were illuminated with a wide-band incoherent white light source, but the light incident on our sensor was spectrally filtered via a 1 nm full width at half-maximum bandpass filter centered at 532 nm wavelength. Each captured image comprised two subimages (Figure 5A). The full scene was then reconstructed by applying a total variation-regularized deconvolution algorithm⁴⁸ to the subimage produced by the EDOF metalens and its measured PSF. After segmenting the reconstructed image and labeling objects for depth estimation, we could estimate the experimental DH-PSF for each object of interest. Figure 5B shows the PSF calculated from the image of a "3" character located 6.5 cm away from the metasurface. With the calculated PSFs, we estimated the depth per object (see Methods for further details). Applying this computational framework, we reconstructed scenes and calculated depth maps for the "3"

character of Figure 5B located at five different depths in the 6.5 to 16.9 cm range (Figure 5D,E).

As the DH-PSF's rotation angle depends on the wavefront's accumulated Gouy phase,^{43,44} off-axis aberrations such as field curvature induce rotation offsets to the PSF that vary as a function of field angle (i.e., the angle to an object in the scene as measured from the optical axis). In a refractive lens system with multiple surfaces that mitigate aberrations from off-axis and offcenter light (e.g., Petzval field curvature, coma), the resulting focal shift and rotation offset are reduced and the depth can be extracted directly from a calibration curve¹³ as in Figure 4C. Our metalens, however, does not correct for these aberrations (Figure S3). Hence, naively treating all field angles in the same manner produces erroneous depth estimates as the focal shift is nonnegligible. To address this, our algorithm accounts for focal shifts induced by off-axis aberrations and correspondingly compensates the rotation angle to improve the depth estimation accuracy by calculating the additional Gouy phase due to field angle (details of the reconstruction and depth estimation algorithm are provided in the Methods and Supporting Information).

For the case of the single object "3" character at five different depths, the accuracy of our estimation is demonstrated in Figure 5C, where the estimated and true depths strongly agree. In this case, accounting for off-axis aberrations had minimal effect, as there was little rotation offset to mitigate because the "3" characters were located near the center of the field of view. We then applied our framework to a scene comprising more than one object located off-axis with higher field angles, consisting of a further located "U" character and a closer "W" character. Here, the captured data (Figure 6A) and the subsequently reconstructed image (Figure 6B) allowed us to estimate distinct double-helix PSFs for each character, shown in Figure 6C and D for the "U" and "W", respectively. A naive depth estimation without accounting for off-axis focal shift yields highly erroneous depth estimates; however, once the change in Gouy phase due to the field angle of each character is compensated for, the estimates agree well with the true depths once again (Figure 6E). With the depth estimates of both Figure 5 and Figure 6, our system achieves a fractional ranging error of 1.7%, higher than but of similar order compared to existing commercial passive depth cameras but with a much more compact form factor.

DISCUSSION

While various depth estimation techniques exist, our method enables 3-D imaging of scenes in an ultracompact form factor without having to take multiple snapshots under different optical configurations. By combining the imaging lens and the wavefront coding steps into a single aperture, the size is reduced significantly, albeit at the cost of introducing off-axis and chromatic aberrations from the metalenses. These aberrations, however, are largely mitigated by limiting the optical bandwidth in detection and accounting for the field angle dependence of the focal length when calculating depths. The form factor reduction will be beneficial for a variety of systems, such as head-mounted displays for augmented reality, which impose stringent size limitations on sensors. Shifting the functionality of the SLM and 4f correlator into the dual-aperture metalens not only contributed to this size reduction but also eliminated the time multiplexing required in previously reported PSF engineering methods.¹³ Eliminating this time multiplexing serves a dual purpose: it reduces the system complexity and circumvents the issue of a scene changing between sequential captures. Although the spatial multiplexing of two metasurfaces does induce parallax, the center-to-center separation of each metasurface poses a negligible angular separation (less than 0.4°) for the average object depth in our experiments. Compared to alternative metasurface-based depth cameras,³⁰ our design accommodates a wider depth range with a smaller aperture and achieves a lower fractional ranging error on our tested scenes, owing to the increased Fisher information⁸ from the double-helix mask. Our approach, however, does rely on an image segmentation step in our deconvolution pipeline that inherently limits the transverse resolution of our depth map, whereas conventional depth from defocus methods and metasurface implementations³⁰ rely on finite differences between images that enable denser depth maps.

We demonstrated a compact and visible wavelength depth camera for three-dimensional imaging based on a dual-aperture optical metasurface. Our system relies on imparting two complementary wavefront coding functions on light from a scene to create an accelerating and a rotating beam, enabling simultaneous focused scene reconstruction at all distances and depth discrimination for objects in the scene with a single image snapshot. Compared to existing implementations of depth cameras, we demonstrated an ultracompact solution with a 2 mm² optical aperture and without requiring a separate imaging lens, 4f correlator, or spatial light modulator. While use of metasurfaces must contend with off-axis aberrations via computational correction and a limited operating bandwidth, recent works demonstrating achromatic lensing^{29,35,49–55}

wide-angle field of view correction by stacking metasurfaces⁵⁶ are feasible routes for circumventing these issues. Alternatively, the demonstrated system could be implemented with a spectral filter located at the camera sensor only for the double-helix metalens instead of for both metasurfaces, thereby enabling capture of broadband light with the cubic metalens for full-color scene reconstruction³⁵ without affecting the acquisition of depth information. Although in this work we focused on the 5 to 35 cm range, applicable to gesture recognition for augmented reality systems, the optical design is readily adaptable to other length scales and operating wavelengths by appropriately tuning the cubic phase strength of the EDOF metalens, aperture size, and focal length.

METHODS

Metasurface Design. To optimize the phase for the doublehelix metalens, a block-iterative weighted projections algorithm⁴⁵⁻⁴⁷ was used that axially constrained the diffracted intensity along the optical axis at eight different parallel planes, decomposed the metasurface mask into a linear combination of Laguerre–Gaussian modes, and enforced a phase-only constraint for the mask (see Supporting Information for additional details of the algorithm). The nanopost designs were first simulated using the Stanford S4 rigorous coupled-wave analysis package³⁹ to extract their transmission coefficients. These coefficients were then assigned to their corresponding diameters and treated as complex amplitude pixels in a custom wave optics MATLAB code to simulate the full designs. The wave optics simulation was based on the angular spectrum method.⁵⁷

Fabrication. Our process began with a cleaved piece of glass from a 100 mm double side polished fused silica wafer. The silicon nitride layer was first deposited via plasma-enhanced chemical vapor deposition at 350 °C. The sample was then spin coated with ZEP 520A, and an 8 nm Au/Pd charge dissipation layer was sputtered on top. Both metasurface patterns were subsequently exposed adjacent to one another using a JEOL JBX6300FS electron-beam lithography system at 100 kV. After stripping the Au/Pd layer, the sample was developed in amyl acetate. A 50 nm layer of aluminum was evaporated and lifted off via sonication in methylene chloride, acetone, and isopropyl alcohol. The silicon nitride layer was then etched with the remaining aluminum as a hard mask using an inductively coupled plasma etcher with a CHF₃ and SF₆ chemistry. The remaining aluminum was finally removed by immersing the sample in AD-10 photoresist developer. An Au/Pd layer was sputtered on top of the sample for charge dissipation when capturing scanning electron micrographs.

Experiment. To measure the point spread functions, a 50 μ m pinhole was aligned with the sample and illuminated from behind with a LED source. For imaging experiments, the pinhole was removed and objects on printer paper were illuminated with a white light LED array panel source. For both the point spread functions and images, the captured signal was limited in bandwidth via a 1 nm full width at half-maximum spectral bandpass filter centered at 532 nm wavelength. The images and PSFs were magnified via a custom relay microscope comprising an objective and tube lens. The experimental setups and corresponding part numbers for components used in this work are shown in Figures S4 and S5 in the Supporting Information for PSF measurement and imaging, respectively. The transmission efficiency was calculated by taking the power ratio of the light on the sensor side of the metasurface to that on the source side. The diffraction efficiency was calculated by taking the ratio

of the power at the metasurface on the sensor side to that at the focal plane. These powers were measured by integrating the intensity within the area of the metasurface aperture from images when it was back-side illuminated.

Deconvolution. The reconstructed scene images are calculated by deconvolving the cubic subimages using a total variation-regularized deconvolution algorithm. This deconvolution problem is solved using an open source MATLAB library based on the split Bregman method,⁴⁸ which iteratively solves the reconstruction problem. After segmenting the reconstructed scene and labeling objects for depth estimation, we applied a Kaiser window in each desired subregion of the image with a labeled object. Subsequent deconvolution of the subregions via a Wiener filter applied to the double-helix subimage provided an estimate of the DH-PSF for each object of interest. With the PSF estimates for each labeled object, the orientation angles of the lobes were extracted and compared against the experimentally calibrated angle response of the DH-PSF as a function of depth (Figure 4C), providing a depth estimate for each object. We calculate the focal shift due to off-axis aberrations by finding ray intersections and determine the subsequent change in Gouy phase and rotation angle by using an ABCD formalism for the Gaussian complex beam parameter (see Supporting Information for details). As scene reconstruction and depth estimation per segmented object average 26.5 and 0.8 s, respectively, using an ordinary personal laptop computer (12 GB RAM, Intel CORE i7) with the algorithm implemented in MATLAB, real-time processing would not be possible, though video data could be processed offline after data capture. Significant speedups to achieve real-time processing are feasible; however, if dedicated hardware were used, such as field-programmable gate arrays or graphics processing units.

ASSOCIATED CONTENT

Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acsphotonics.0c00354.

Nanopost design and the validity of the unit cell approximation; high-efficiency double-helix PSF phase mask optimization; validity of superposing phase masks for point spread function engineering; scene reconstruction algorithm; depth estimation algorithm; correcting depth estimates for nonzero field angles; PSF measurement setup; imaging setup; modulation transfer functions; Fisher information with depth (PDF)

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Notes

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