

# **Models are Always Wrong, Right? What's the Difference Between an \$85 Model and a \$2,000,000 Model**

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April 4, 2002

# Australia, not Austria



# Australia, not Austria



# Taz



Taz

# Tassie, not Taz



Taz

# Laws of Simulation and Modeling

- **A simulation is only as accurate as the models it is based on**
- **A model is (mostly) useless unless it is embedded in a simulator**
- **Models are, by definition, inaccurate; it's just a matter of degree**
- **Models generally trade off complexity (simulation time) for accuracy**

# Zeroeth Law of Modeling

**Physics (reality)  
trumps  
Mathematics**

# Zeroeth Law of Modeling

**Measurements  
trump  
Models**

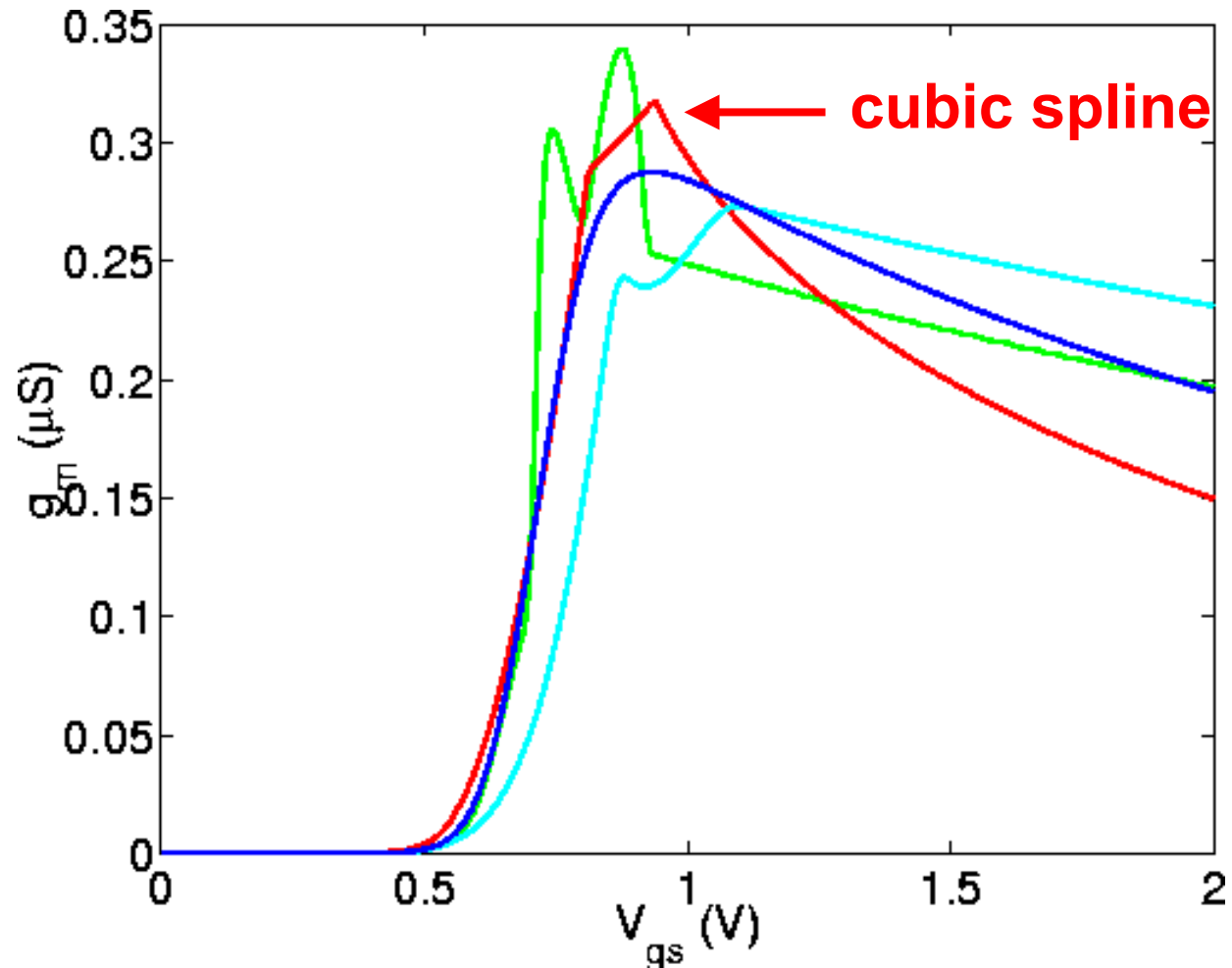


# Zeroeth Law of Modeling

# Measurements trump Models

Especially when Engineers Use Polynomials

# Numerical Tricks May not Work

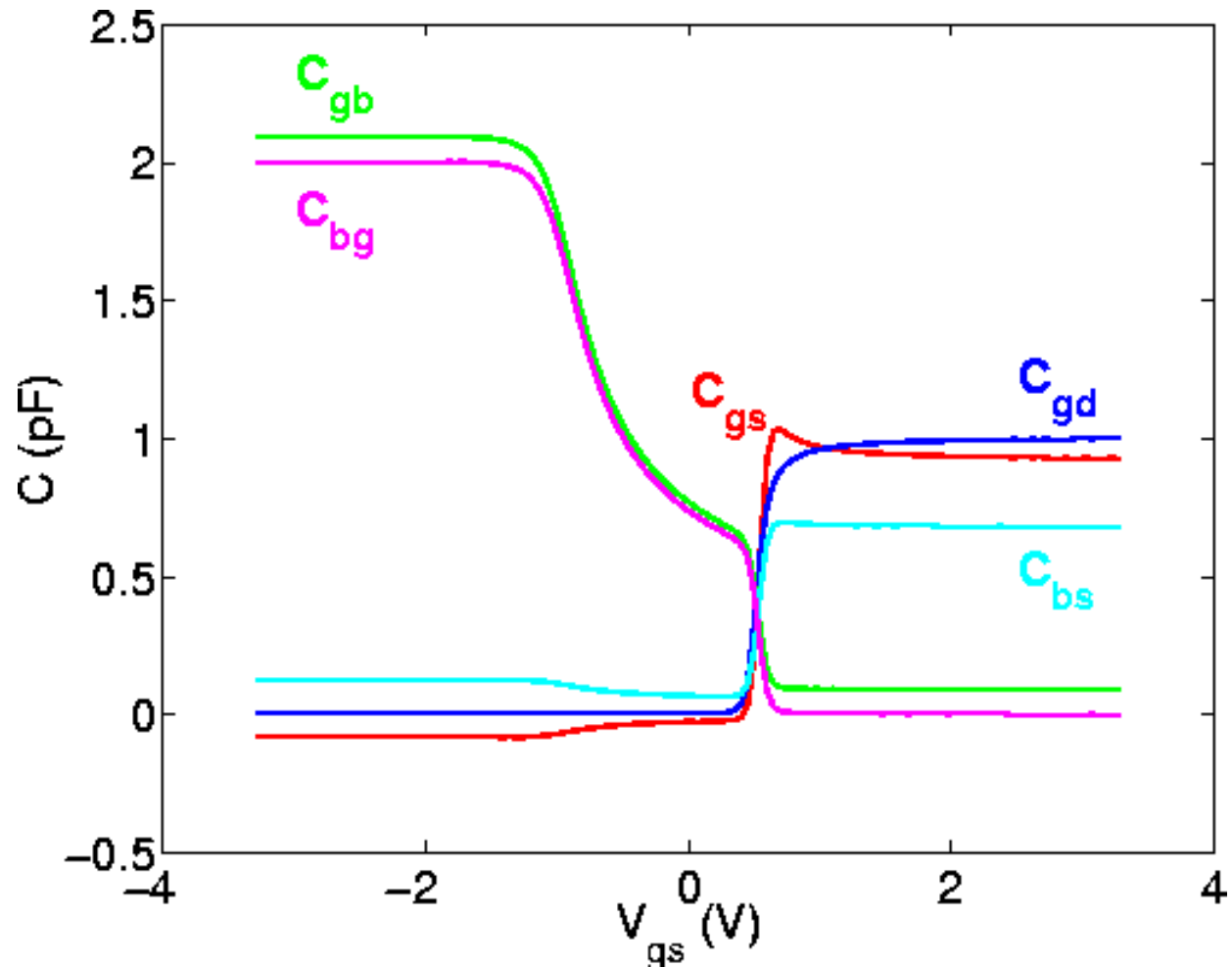


# Zeroeth Law of Modeling

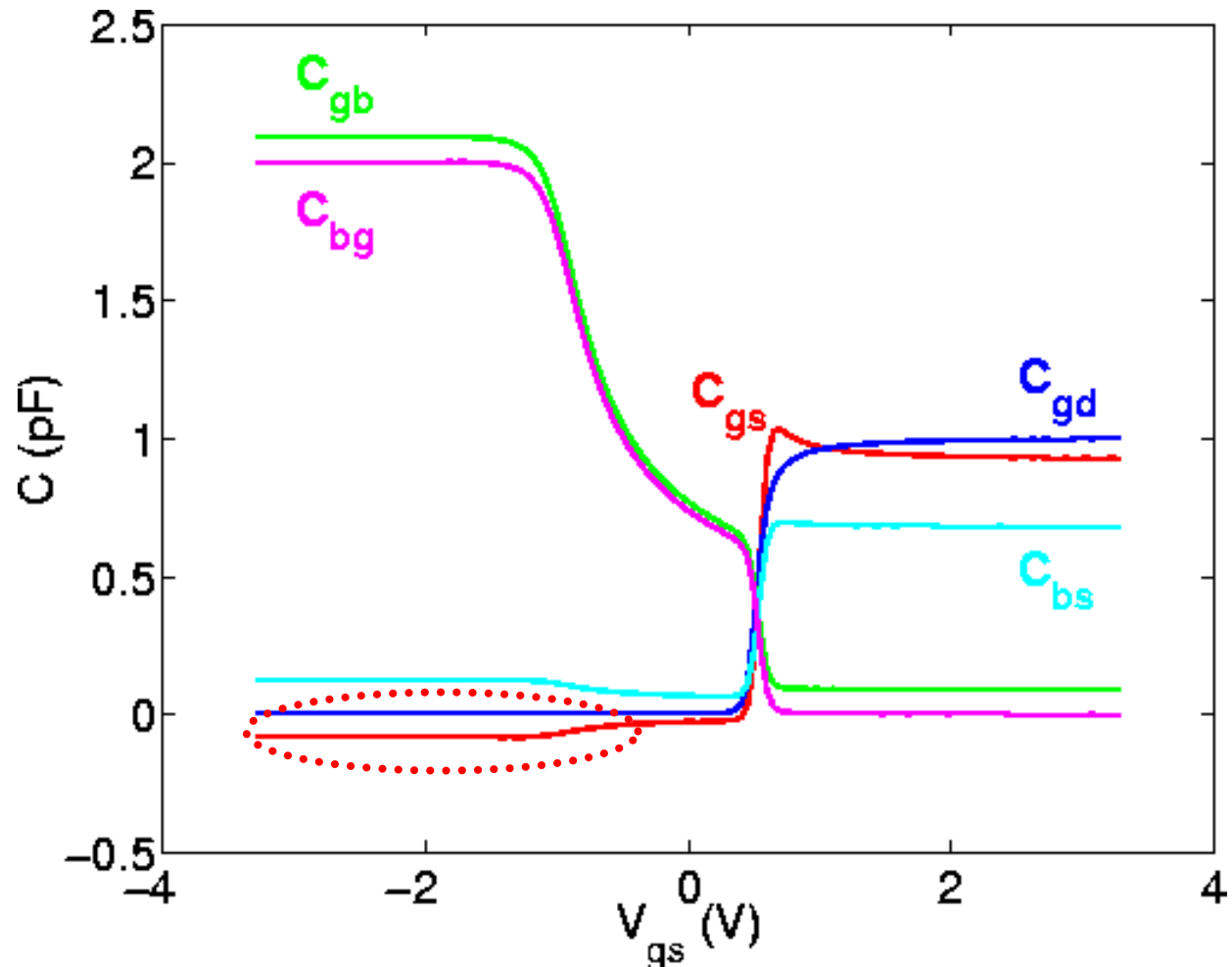
**Measurements  
trump  
Models**

**Just be careful you know what you are measuring**

# Negative Capacitance Bloop



# Negative Capacitance Blooper



# Simple way to Get Capacitance

- Terminal currents from AC analysis

$$i_i = (g_{ik} + j\omega C_{ik})v_k$$

- Sequentially excite terminals  $k$  with  $1+j0$  volts at  $\omega=1$ , i.e.  $f=1/(2\pi)$

$$C_{ik} = \text{im}(i_i)$$

- Change sign if  $i \neq k$

# Oz is Acceptable

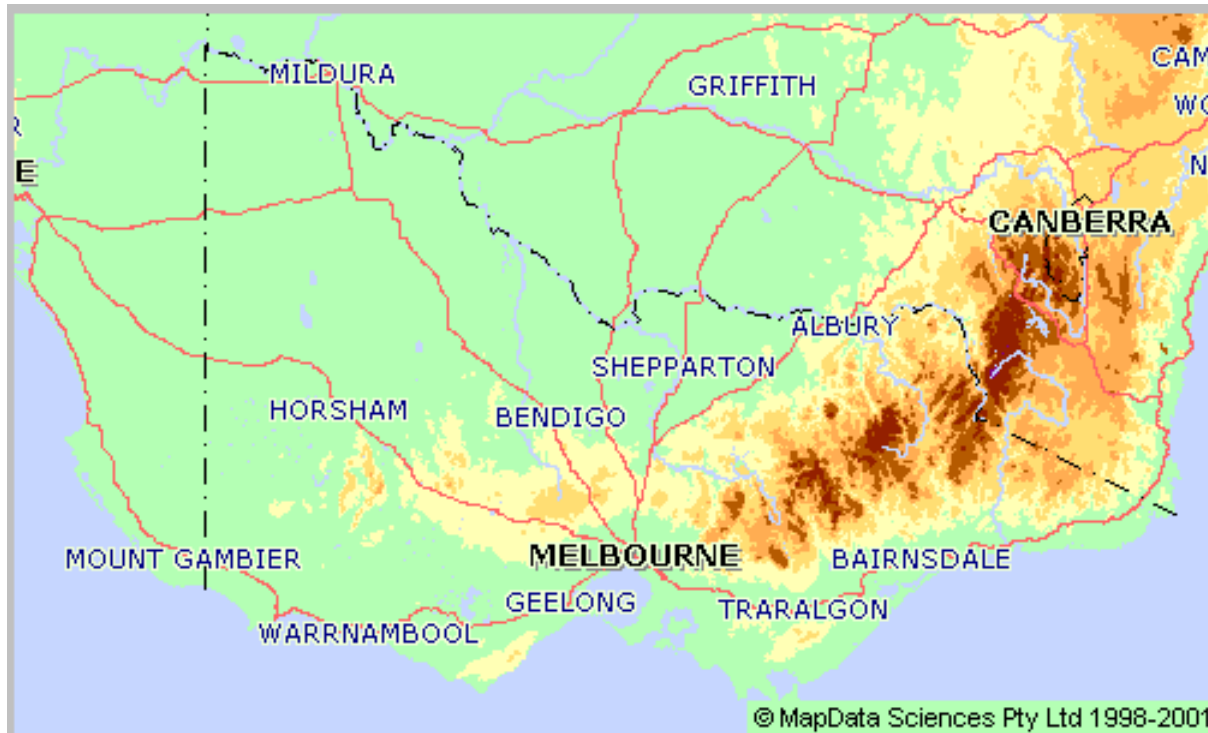


# Aussie, not Ozzie





# Victoria



# Charge or Capacitance?

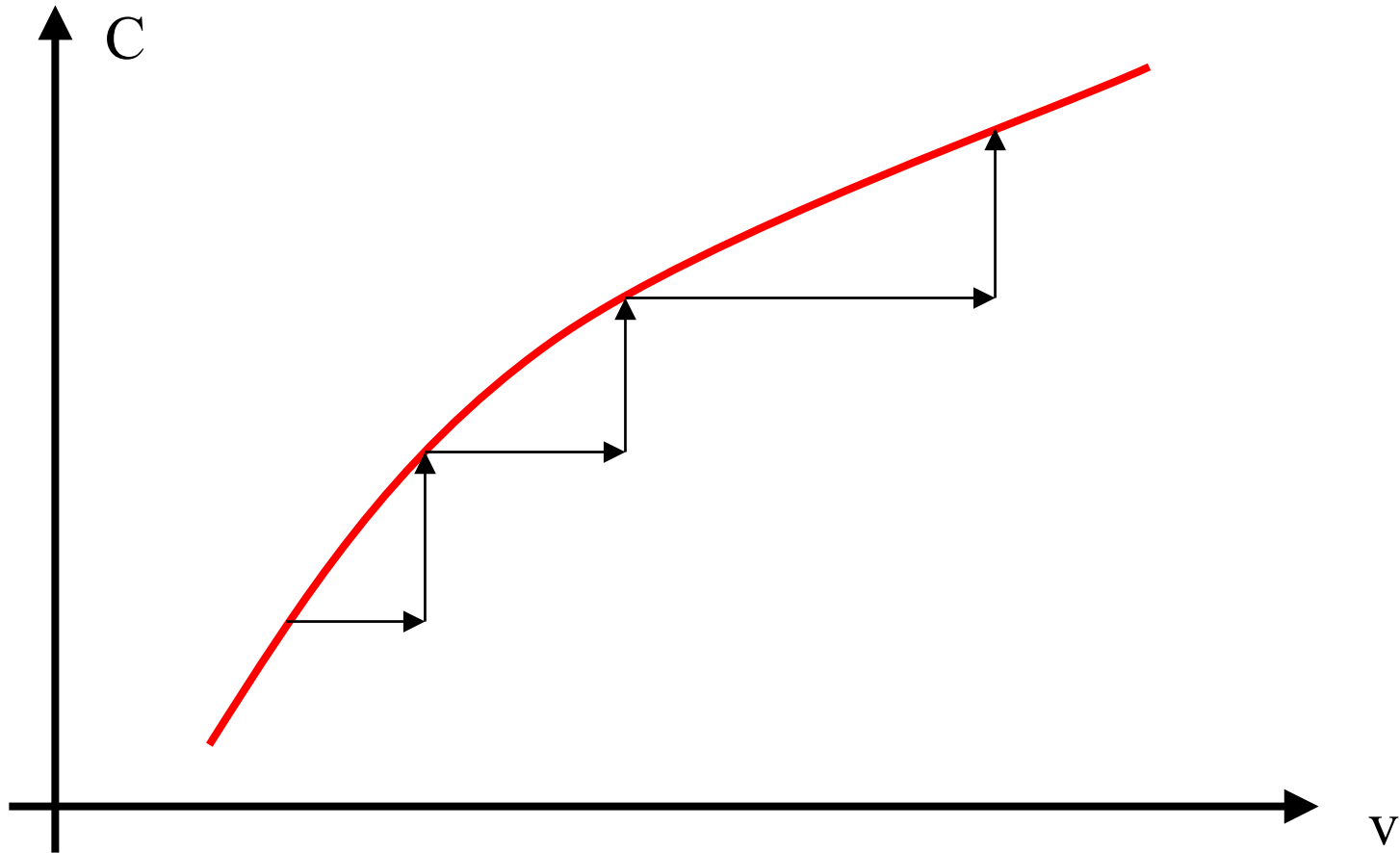
- They're really the same, right?

$$q = Cv(t)$$

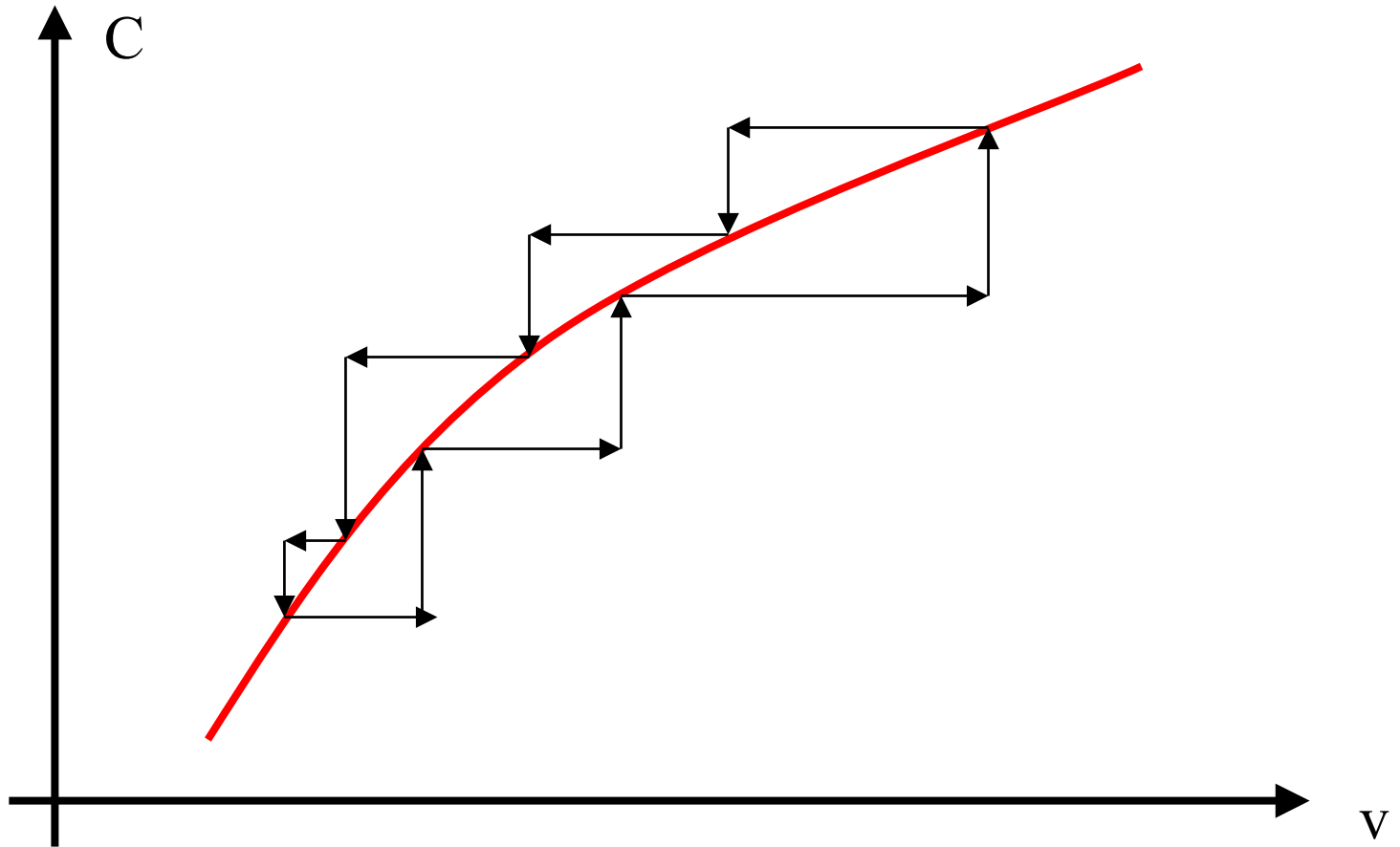
$$i = \frac{\partial q}{\partial t} = \frac{q_{k+1} - q_k}{t_{k+1} - t_k}$$

$$i = C \frac{\partial v}{\partial t} \approx C_k \frac{v_{k+1} - v_k}{t_{k+1} - t_k}$$

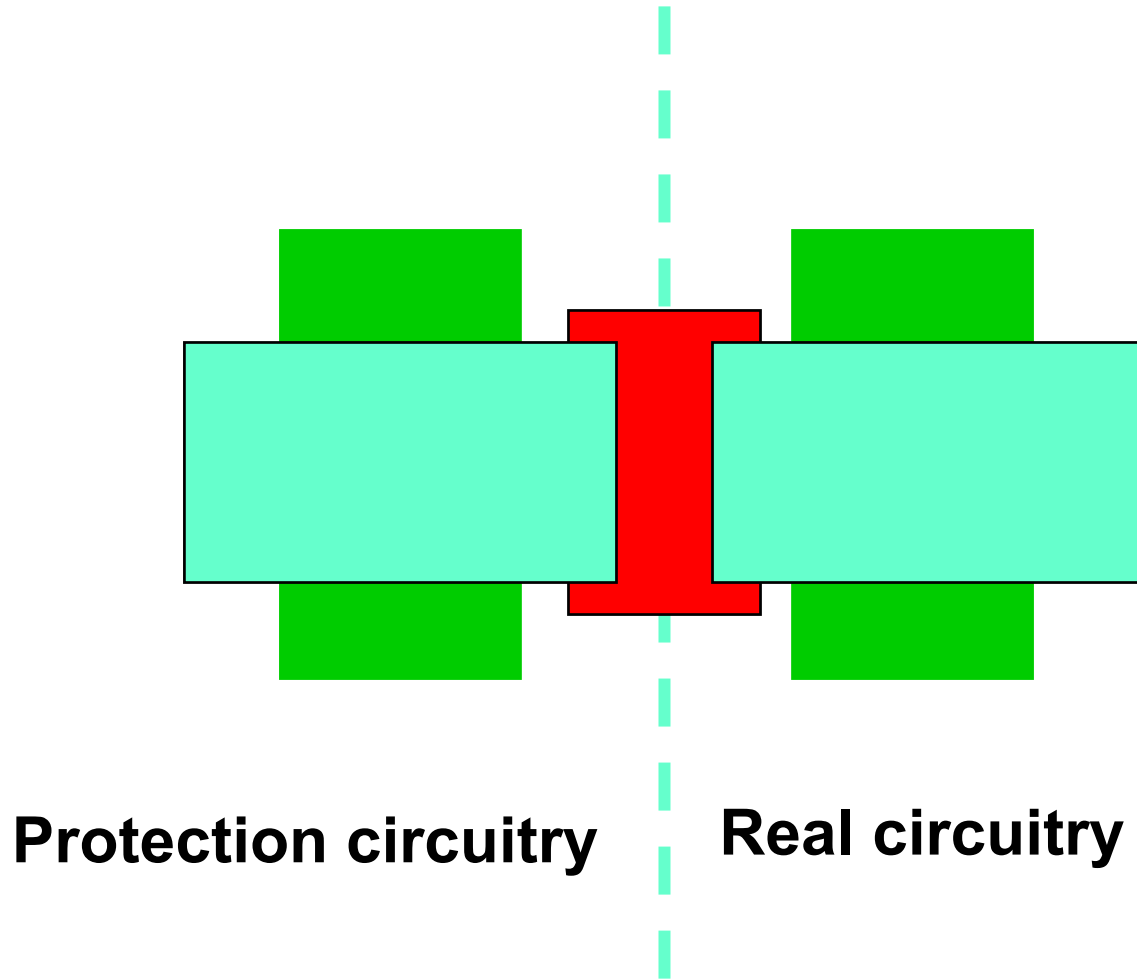
# Charge or Capacitance?



# Charge or Capacitance?



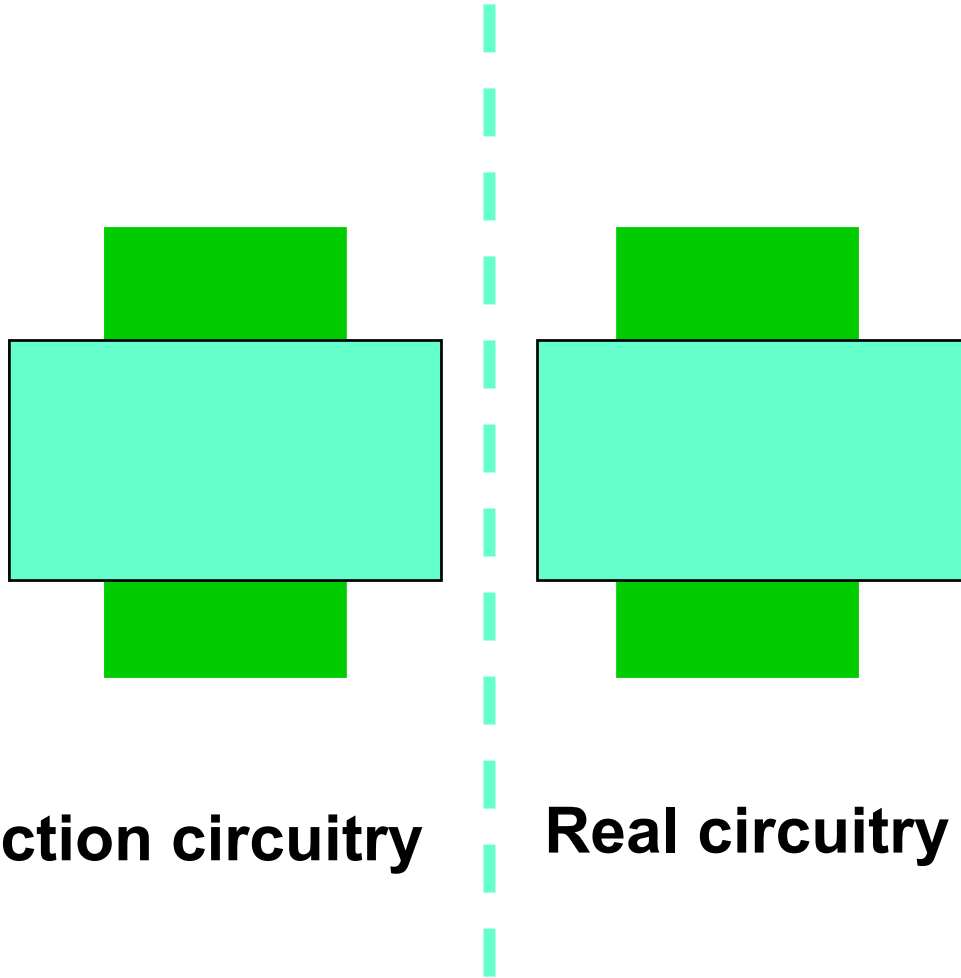
# Will the IC Fail?



**Protection circuitry**

**Real circuitry**

# Metal Routing Missing



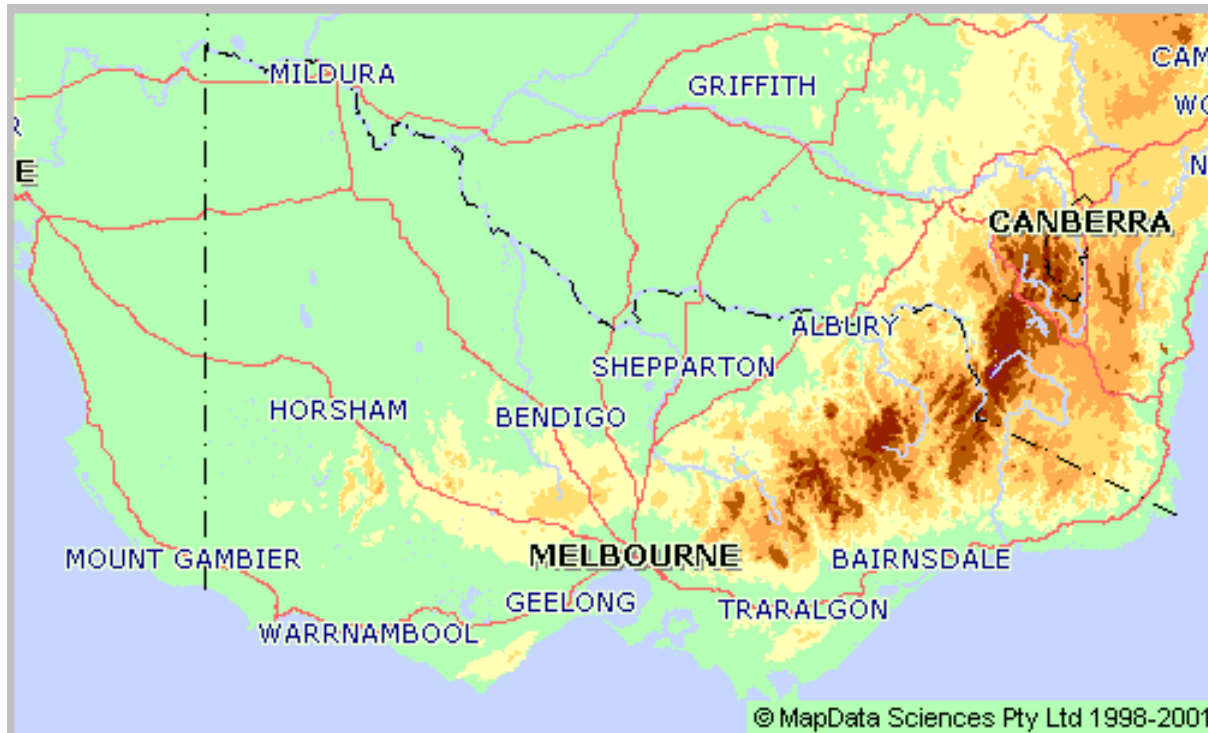
**Protection circuitry**

**Real circuitry**

# Simulation Results

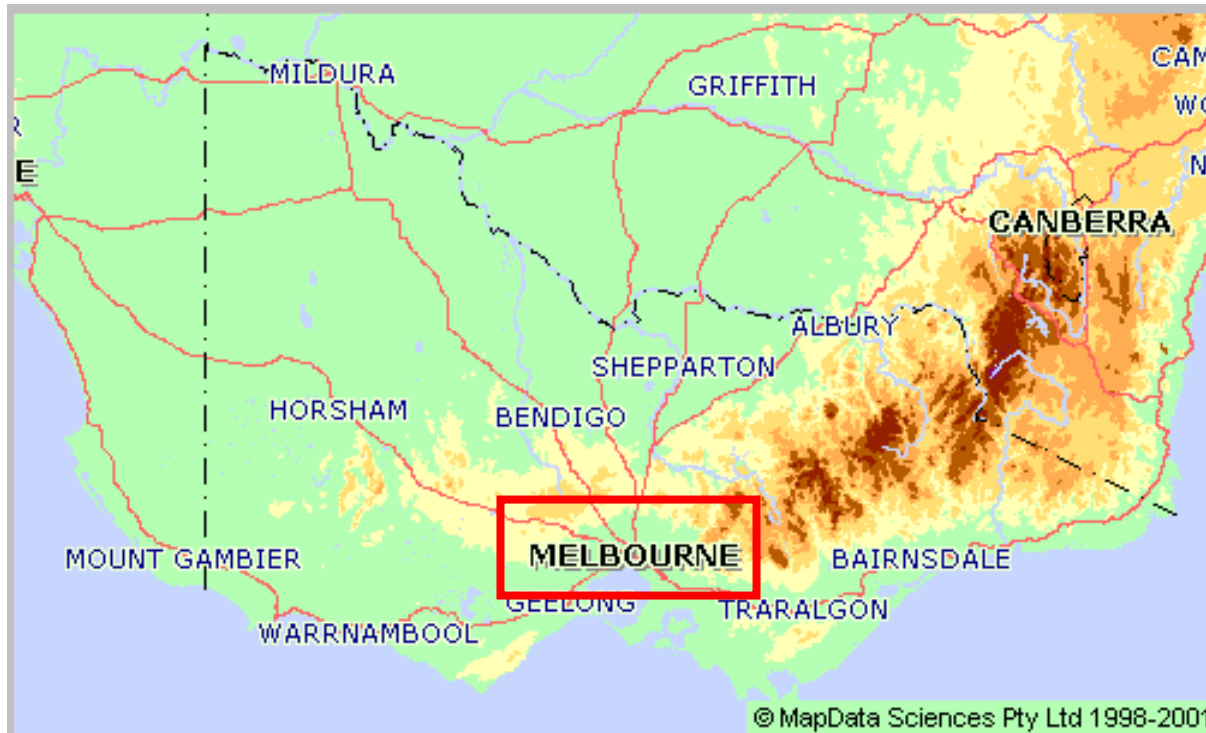
- **Capacitance based model did not conserve charge, isolated protection circuitry voltage ramped to infinity!**
- **Charge based model showed the missing metal would **NOT** cause the protection circuitry to trigger**
- **\$2,000,000** of already manufactured parts were shipped and not scrapped

# Victoria





# Victoria



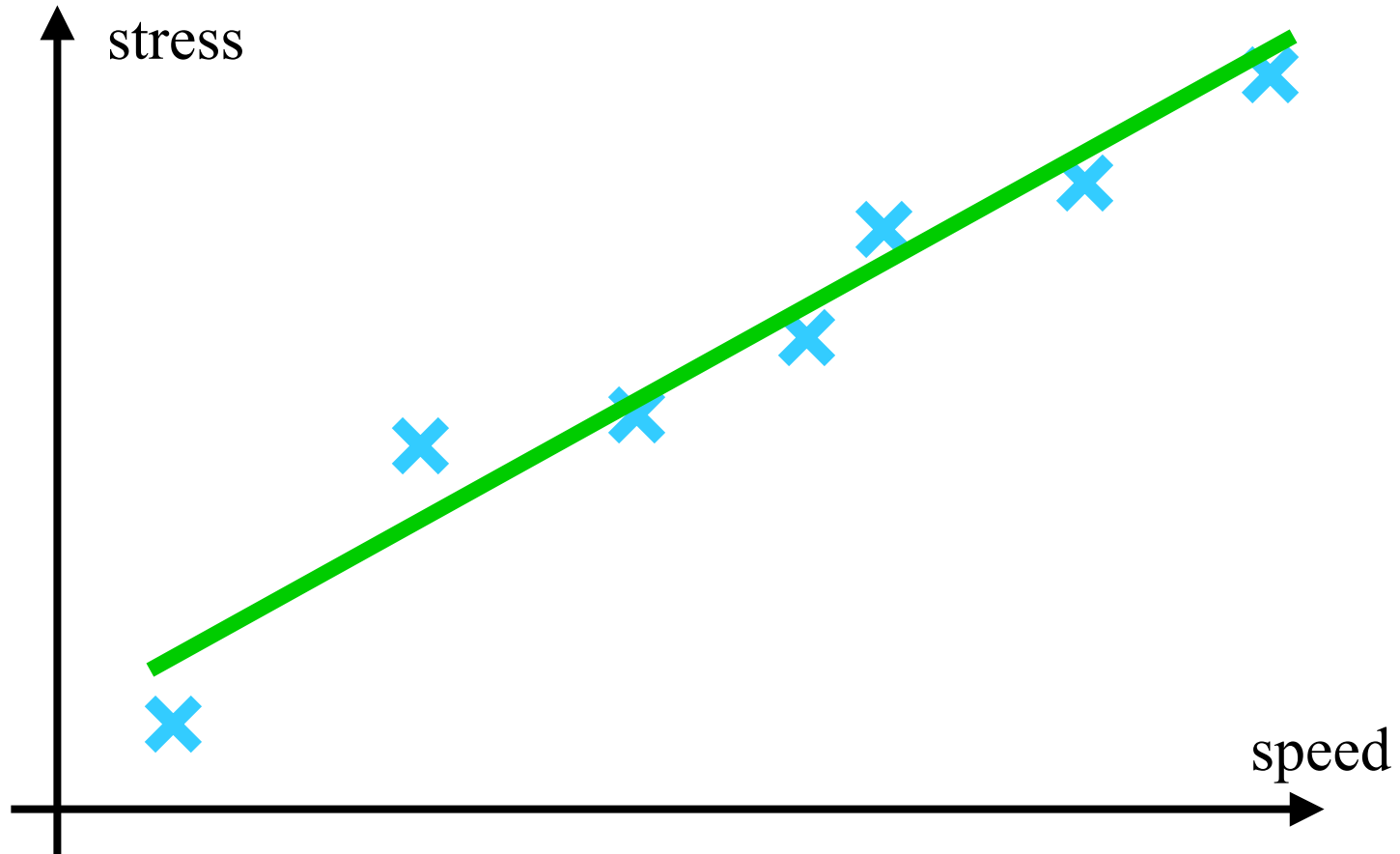
# Melb'n, not Mell-born



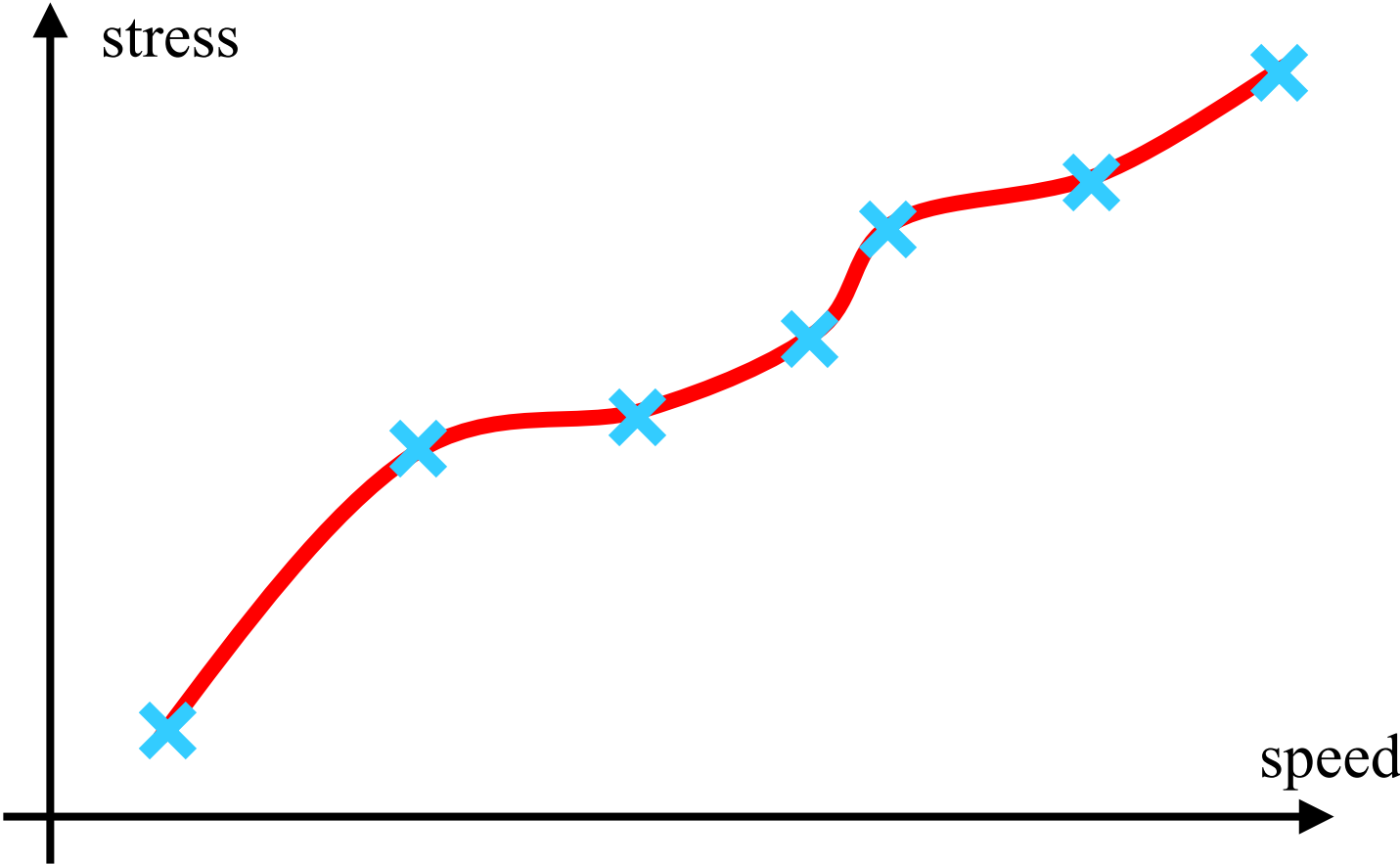
# Milling Coal for the SECV



# Milling Coal for the SECV



# Milling Coal for the SECV



# Melb'n, not Mell-born



# Melb'n, not Mell-born



# Eastern Suburbs





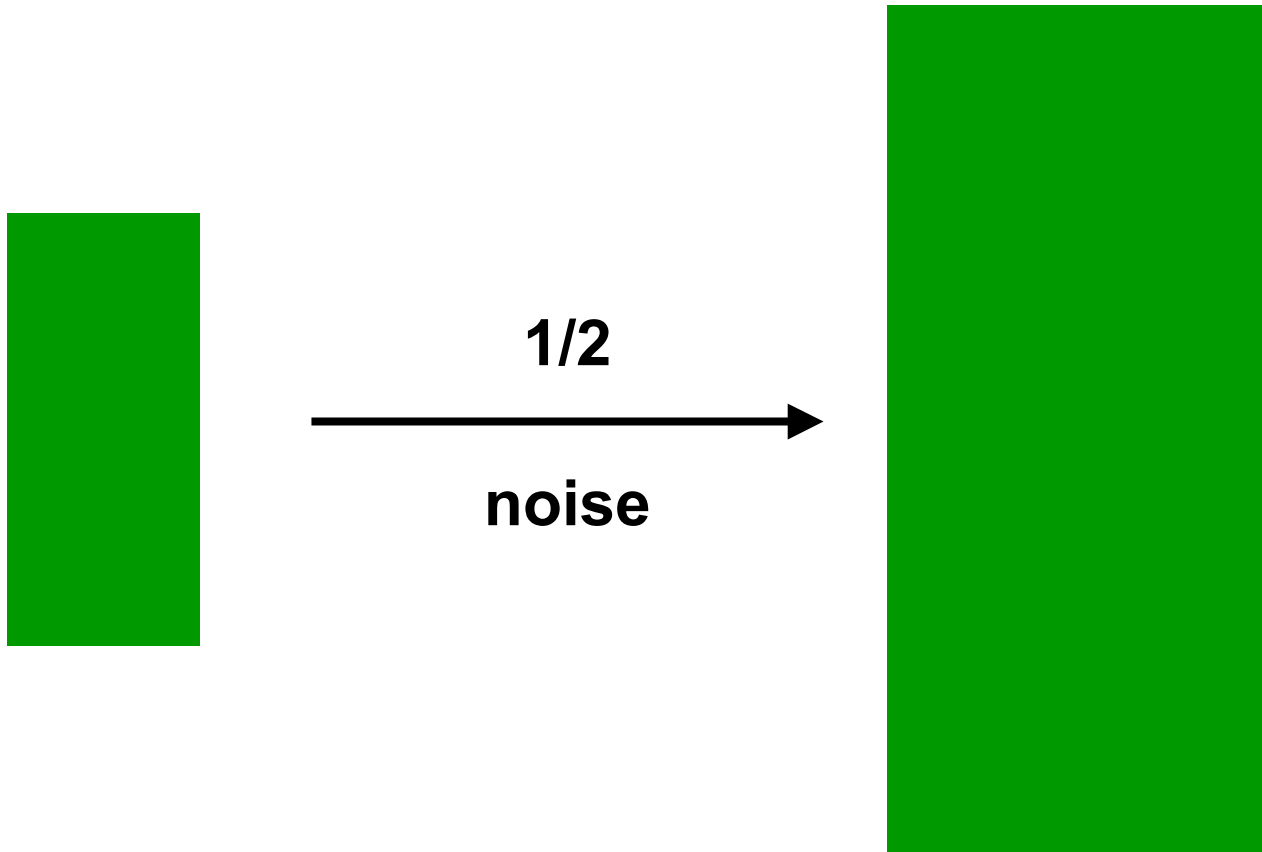
# Asymptotic Correctness

- **Any model should give physically correct and reasonable behavior as any controlling parameter approaches an extreme**
  - Temperature going very cold or hot
  - Geometry getting very large
- **It is amazing how infrequently this simple principle is applied**
  - $1/W$  and  $1/L$  preferred to  $L$  and  $W$

# Universal SPICE 1/f Noise Model

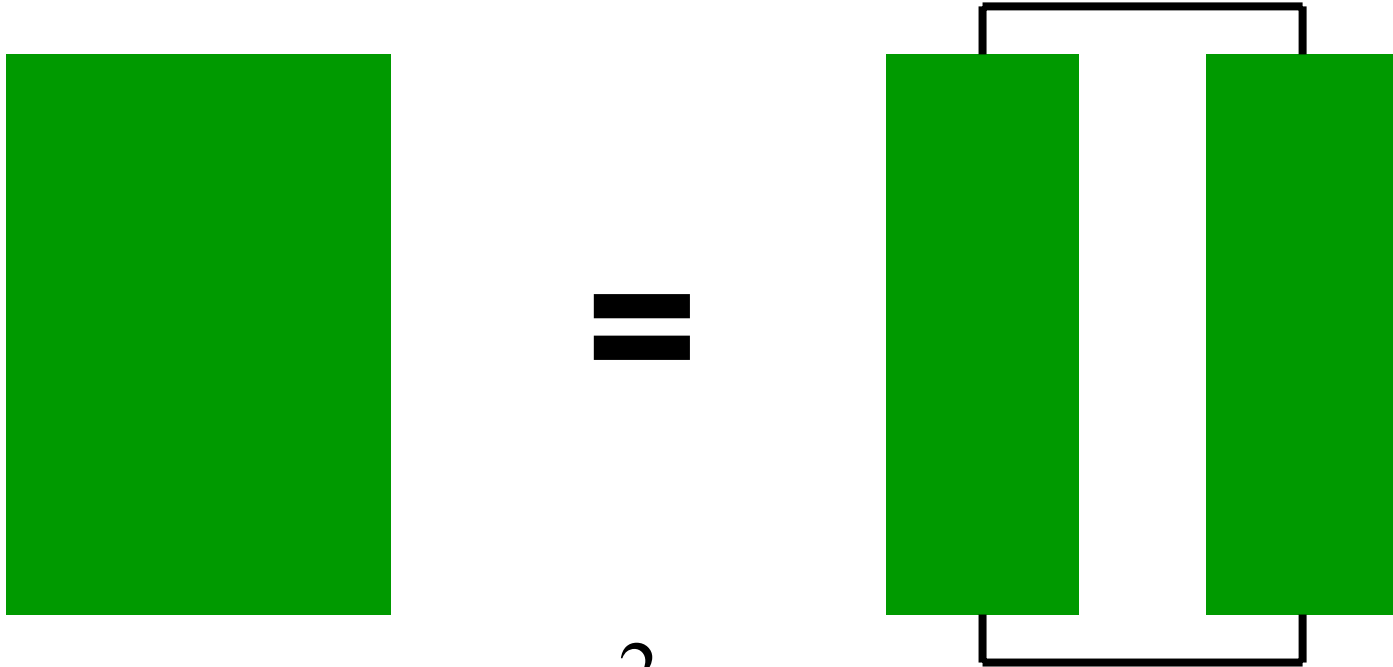
$$\frac{\Delta i^2}{\Delta f} = \frac{K_F (I_{ds})^{A_F}}{LWf}$$

# Universal SPICE 1/f Noise Model



(at a fixed total current)

# Universal SPICE 1/f Noise Model



$$\frac{\Delta i^2}{\Delta f} \propto W$$

# Universal SPICE 1/f Noise Model

$$\frac{\Delta i^2}{\Delta f} = \frac{K_F (I_{ds})^{A_F}}{L W f}$$

$$I_{ds} = I_{ds}^0 \frac{W}{L}$$

$$\frac{\Delta i^2}{\Delta f} = \frac{K_F W^{A_F - 1} (I_{ds}^0)^{A_F}}{L^{A_F + 1} f}$$

# Symmetry

- Most MOSFET and resistor models are cast in the form  $I_{ds} = G V_{ds}$
- $G(V_{sb}, V_{db}, V_{gb})$  is the effective conductance of the MOSFET or resistor
- Consider symmetric biasing  
 $V_{db} = V_{db0} + V_x$ ,  $V_{sb} = V_{sb0} - V_x$ ,  $V_{ds} = 2V_x$
- $I_{ds}$  **MUST** be an odd function of  $V_x$
- $G$  **MUST** be an even function of  $V_x$
- Limiting of  $V_{ds}$  to  $V_{sat}$  **MUST** be odd

# Eastern Suburbs

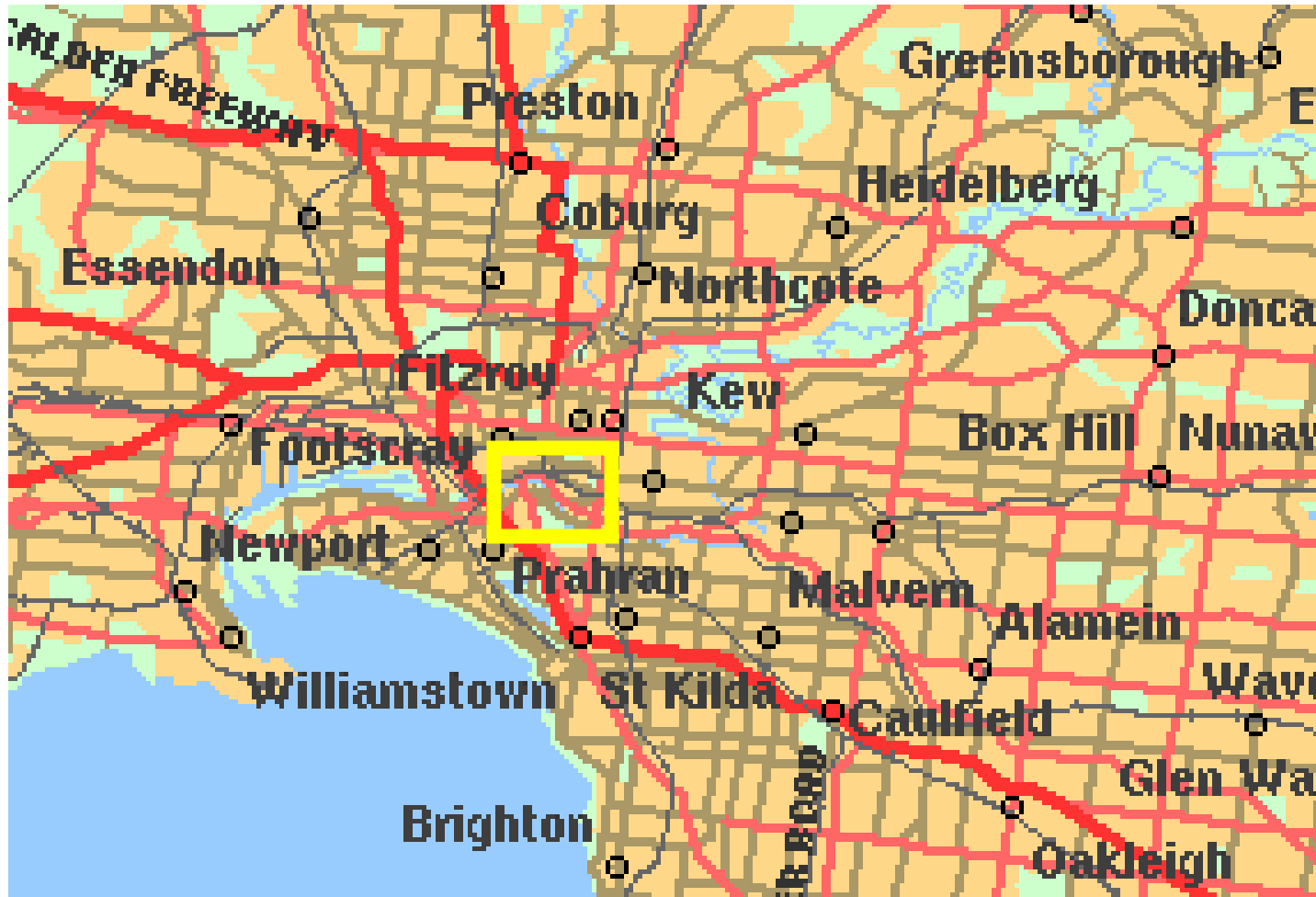


# Eastern Suburbs





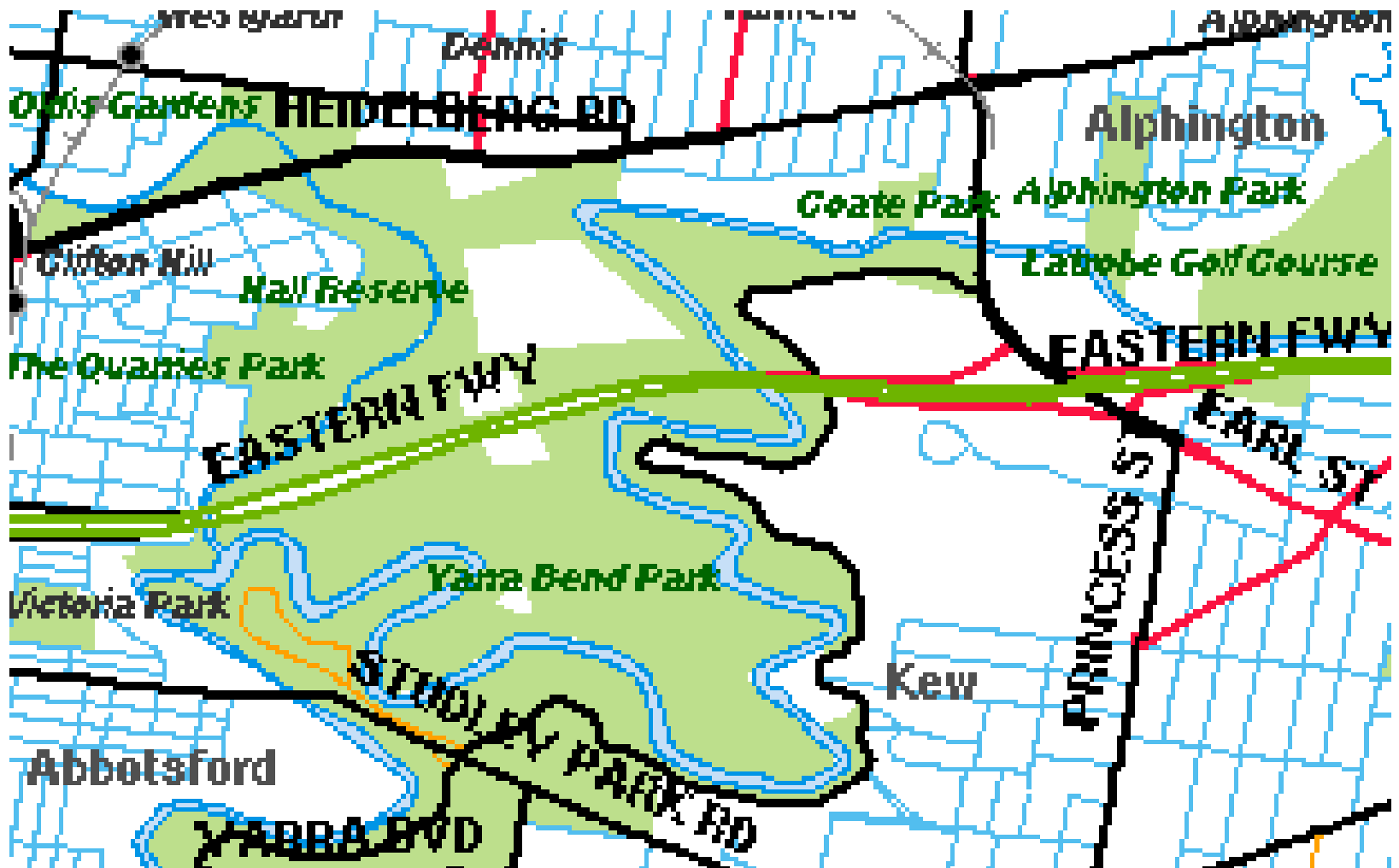
# Eastern Suburbs



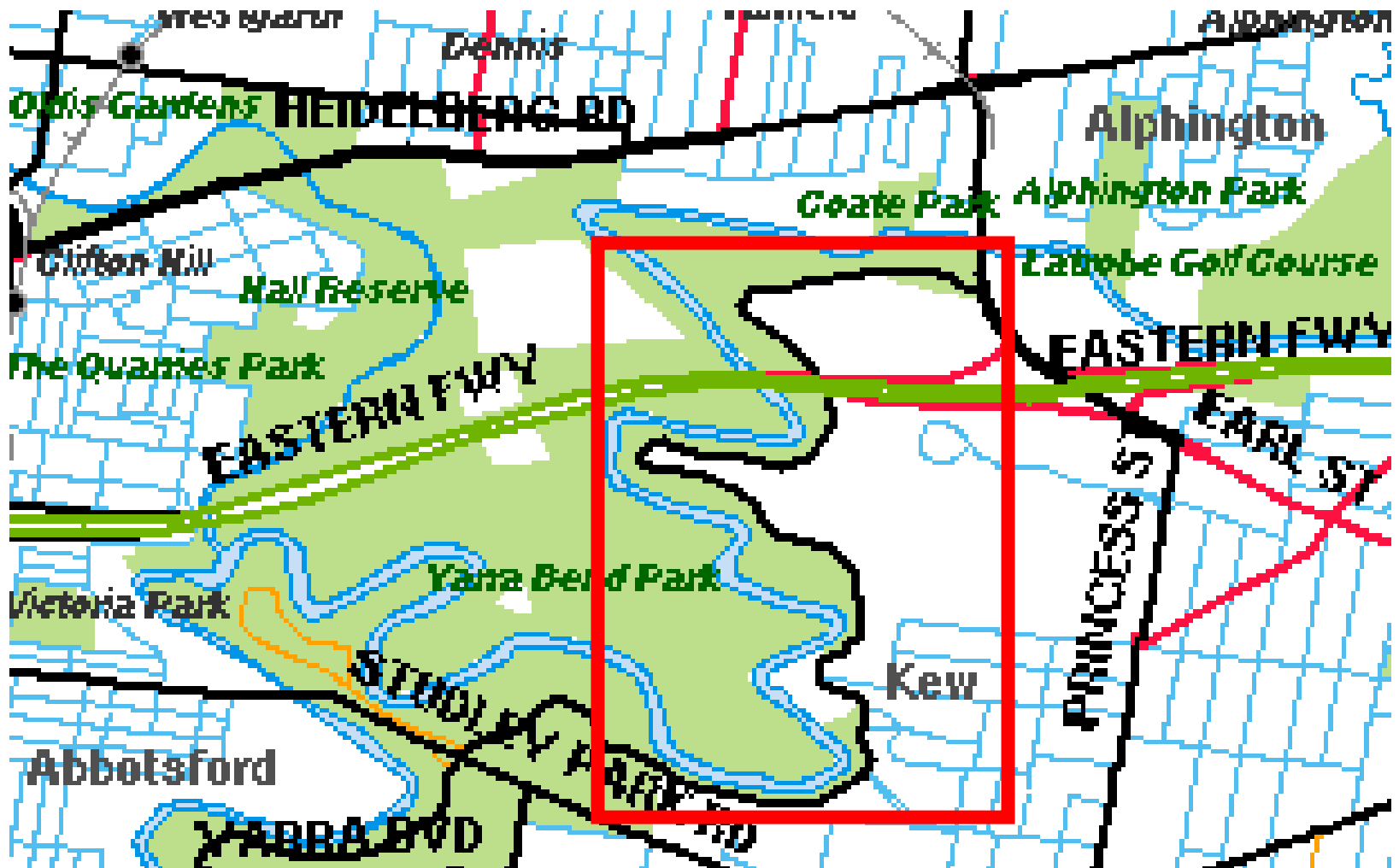
# Eastern Suburbs



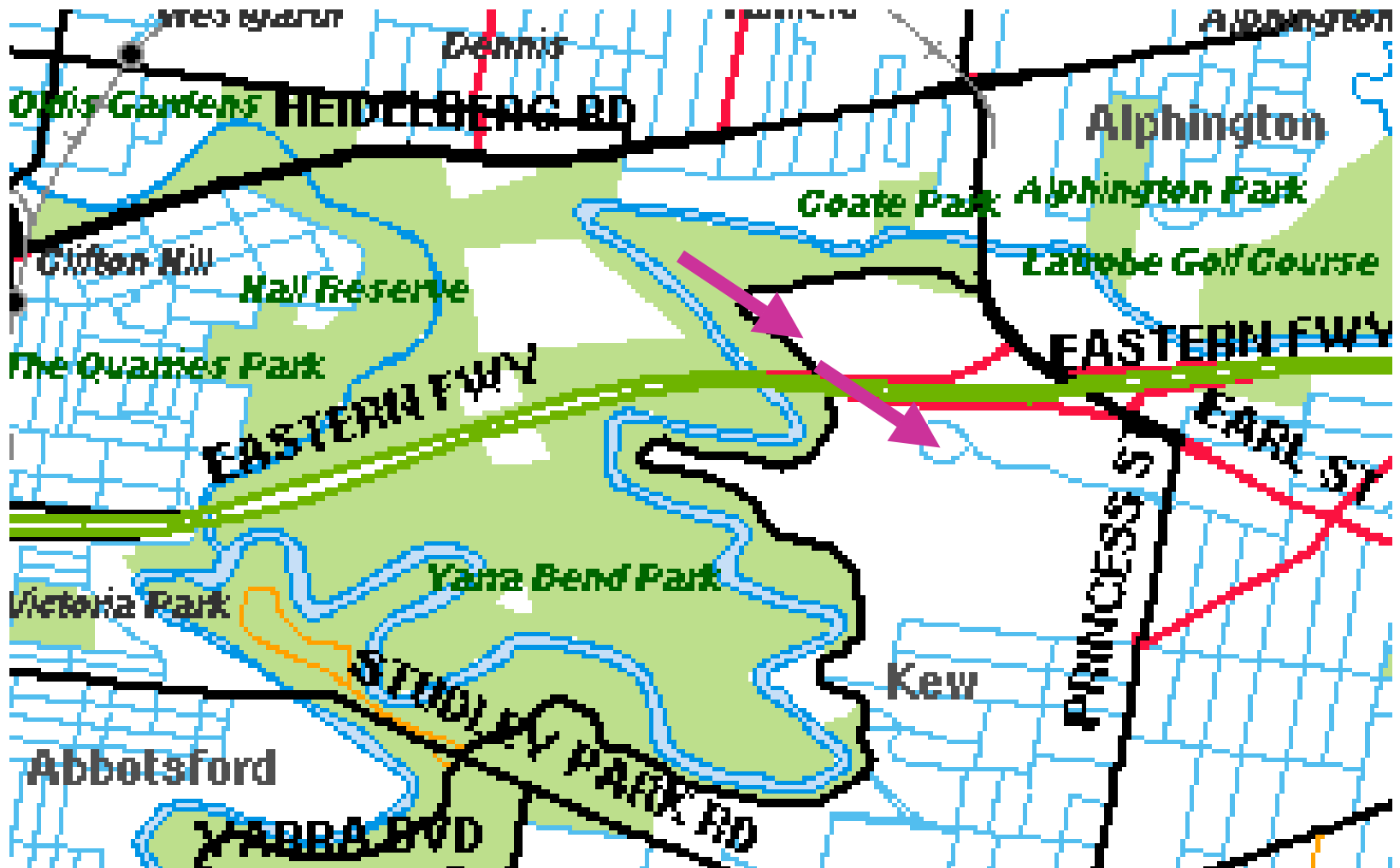
# Kew



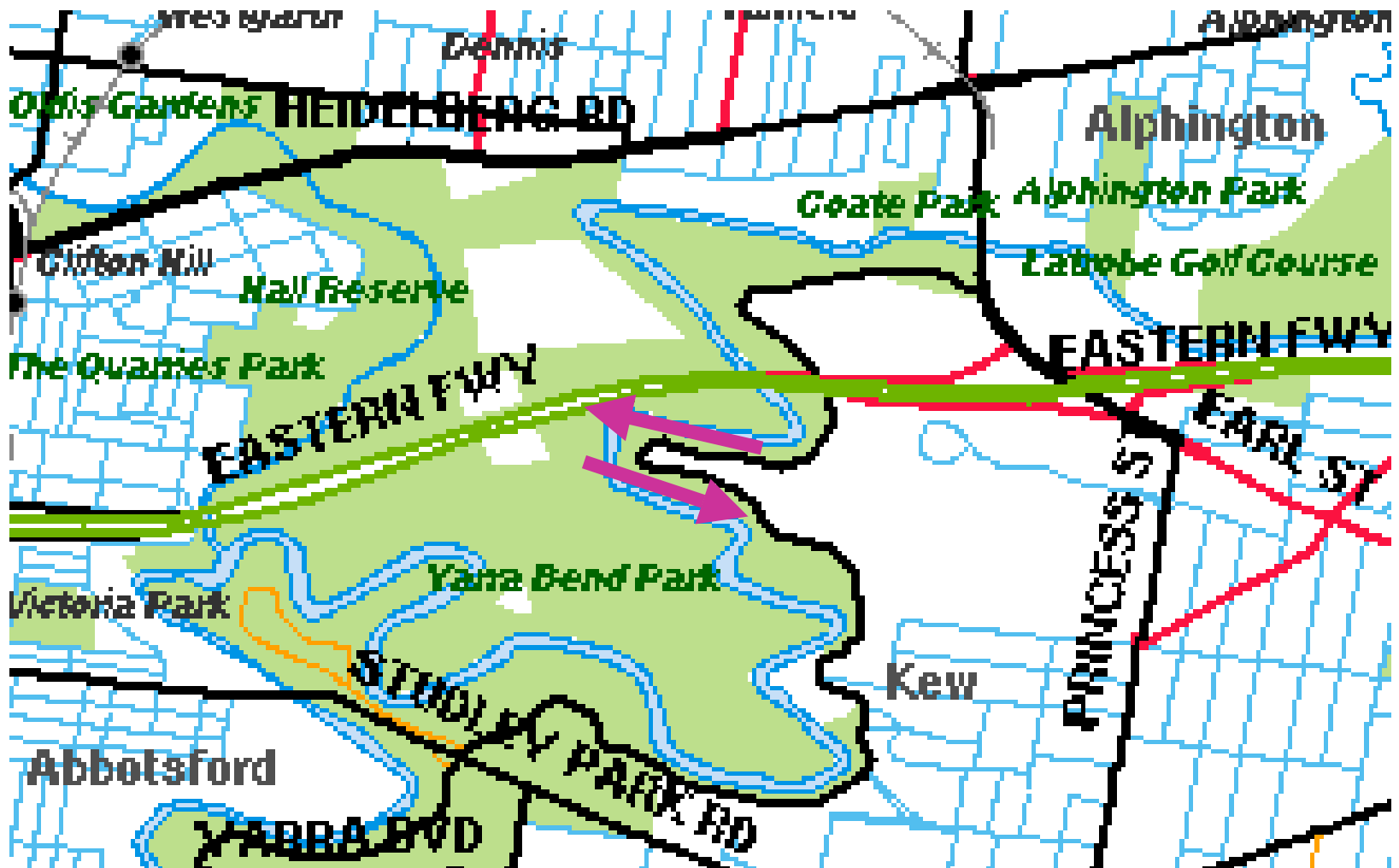
# Kew



# Kew



# Kew



# Kew

